# Vector Calculus

## **Vector Fields**



Chapter 14 will examine a vector field.

For example, if we examine the temperature conditions in a room, for every point P in the room, we can assign an air temperature, T, where

$$T = f(x, y, z)$$

This is a scalar function or scalar field.

However, suppose air is moving around in the room and at every point P, we can assign an air velocity vector,  $\vec{V}(x, y, z)$ , where

$$ec{V}(x,y,z) = \hat{i} \ u(x,y,z) + \hat{j} \ v(x,y,z) + \hat{k} \ w(x,y,z)$$

where the right side of the above equation consists of x, y, z components at a point, with each component being a function of (x, y, z). To describe  $\vec{V}$  in the room, we need to keep track of the 3 scalar function, u, v, w at each f(x, y, z).

 $ec{V}(x,y,z)$  is a vector function or a vector field.



z

P

٧

The basic operator is the del operator given as

**2D** 

$$abla = \hat{i}rac{\partial}{\partial x} + \hat{j}rac{\partial}{\partial y} + \hat{k}rac{\partial}{\partial z}$$
 $abla = \hat{i}rac{\partial}{\partial x} + \hat{j}rac{\partial}{\partial y} + \hat{k}rac{\partial}{\partial z}$ 

The del operator operates on a scalar function, such as T = f(x, y, z) or on a vector function, such as  $\vec{F} = \hat{i}P + \hat{j}Q + \hat{k}R$  (force) or  $\vec{V} = \hat{i}u + \hat{j}v + \hat{k}w$  (velocity).

We will examine three operations is more detail

1. gradient:  $\nabla$  operating on a scalar function

Examples include the temperature in a 2D plate, T = f(x, y)

$$abla T = \hat{i} rac{\partial f}{\partial x} + \hat{j} rac{\partial f}{\partial y}$$

or for a 3D volume, such as a room

$$abla T = \hat{i}rac{\partial f}{\partial x} + \hat{j}rac{\partial f}{\partial y} + \hat{k}rac{\partial f}{\partial z}$$

The physical meaning was given in Chapter 13.  $\nabla T$  is a vector perpendicular to the T contours that points "uphill" on the contour plot or level surface plot.

2. divergence:  $\nabla$  dotted with a vector function  $\rightarrow \nabla \cdot \vec{V}$ 

We can define the velocity in a 3D room as

$$ec{V}(x,y,z) = \hat{i}u(x,y,z) + \hat{j}v(x,y,z) + \hat{k}u(x,y,z)$$

DIVERGENCE of  $\vec{V} = \operatorname{div} \vec{V} = \nabla \cdot \vec{V}$ 

$$abla \cdot ec V = \left( \hat{i} rac{\partial}{\partial x} + \hat{j} rac{\partial}{\partial y} + \hat{k} rac{\partial}{\partial z} 
ight) \, \cdot \, \left( \hat{i} u + \hat{j} v + \hat{k} w 
ight) = rac{\partial u}{\partial x} + rac{\partial v}{\partial y} + rac{\partial w}{\partial z}$$

The DIVERGENCE of a vector is a scalar.

3. curl: the vector product of the del operator and a vector,  $\nabla \times \vec{V}$ , produces a vector

$$\operatorname{curl}\operatorname{of}ec{V}=\operatorname{curl}ec{V}=
abla imesec{V}$$

$$egin{aligned} 
abla imes ec{V} &= \left( \hat{i} \, rac{\partial}{\partial x} + \hat{j} \, rac{\partial}{\partial y} + \hat{k} \, rac{\partial}{\partial z} 
ight) imes \left( \hat{i}u + \hat{j}v + \hat{k}w 
ight) \ &\equiv \left| egin{aligned} \hat{i} & \hat{j} & \hat{k} \ rac{\partial}{\partial x} & rac{\partial}{\partial y} & rac{\partial}{\partial z} \ u & v & w \end{array} 
ight| \ &= \left| \hat{i} \left( rac{\partial w}{\partial y} - rac{\partial v}{\partial z} \ rac{\partial}{V_1} 
ight) + \hat{j} \left( rac{\partial u}{\partial z} - rac{\partial w}{\partial x} \ rac{\partial}{V_2} 
ight) + \hat{k} \left( rac{\partial v}{\partial x} - rac{\partial u}{\partial y} \ rac{\partial v}{V_3} 
ight) \ &= \left| \hat{i} \, V_1 + \hat{j} \, V_2 + \hat{k} \, V_3 \end{aligned} \end{aligned} \end{aligned}$$

The **3D** case gives

$$\operatorname{curl} ec{V} = \hat{i} \left( \underbrace{rac{\partial w}{\partial y} - rac{\partial v}{\partial z}}_{V_1} 
ight) + \hat{j} \left( \underbrace{rac{\partial u}{\partial z} - rac{\partial w}{\partial x}}_{V_2} 
ight) + \hat{k} \left( \underbrace{rac{\partial v}{\partial x} - rac{\partial u}{\partial y}}_{V_3} 
ight)$$

The **2D** case gives

$$\operatorname{curl}ec{V} = \hat{k}\left(rac{\partial v}{\partial x} - rac{\partial u}{\partial y}
ight)$$

4. Laplacian:  $(\nabla \cdot \nabla)$  operation.

A primary example of the Laplacian operator is in determining the conduction of heat in a solid. Given a 3D temperature field T(x, y, z), the Laplacian is

$$rac{\partial^2 T}{\partial x^2}+rac{\partial^2 T}{\partial y^2}+rac{\partial^2 T}{\partial x^2}=0$$

#### 2D example

Consider a 2D heat flow field,  $\vec{q}(x, y)$ .

Look at a small differential element,  $\Delta x \Delta y$ . In steady state, heat flows in is equivalent to heat flow out. Therefore

$$\nabla \cdot \vec{q} = 0 \qquad (1)$$

But  $\vec{q}$  is related to temperature by Fourier's law

$$\vec{q} = -k\nabla T$$
 (2)

Combining (1) and (2)

$$abla \cdot (-k 
abla T) = 0 
ightarrow 
abla^2 T = 0$$

This is Laplace's equation in 2D, which gives the steady state temperature field.

## Example 4.1

Show for the 3D case f(x, y, z) that  $\operatorname{curl}\operatorname{grad} f = 0$ 

$$abla f = \hat{i}rac{\partial f}{\partial x} + \hat{j}rac{\partial f}{\partial y} + \hat{k}rac{\partial f}{\partial z}$$

holds for any function f(x, y, z), for instance

$$f(x, y, z) = x^2 + y^2 + y \sin x + z^2$$

#### Conservative Force Fields and the $\operatorname{curl} \operatorname{grad} f = 0$ identity

Suppose we have a conservative field  $\vec{F}(x, y, z)$ . We know  $\vec{F}$  is irrotational, i.e.

$$abla imes ec{F} = 0$$
 (1)

(zero work in a closed path in the field)

But the identity says

$$abla imes (
abla \phi) = 0$$
 (2)

always holds when  $\phi(x, y, z)$  is a scalar function.

Comparing (1) and (2)  $\rightarrow$  for a Conservative Force Field, we can always find a scalar function  $\phi(x, y, z)$  such that

$$ec{F} = oldsymbol{
abla} \phi$$

where  $\phi$  is called the scalar potential function.

Sometimes, for convenience, we introduce a negative sign

$$ec{F}=-
abla u$$

The following statements are equivalent

 $\vec{F}$  is a conservative  $\iff$  net work when a particle moves through force field  $\vec{F}$  around a closed path in space is zero

 $\iff \nabla imes ec{F} = 0$  irrotational

 $\iff$  a scalar function  $\phi(x, y, z)$  can be found such that  $\vec{F} = \nabla \phi$  or a function u(x, y, z) can be found such that  $\vec{F} = -\nabla u$ 

## Line Integrals of Scalar Functions

The second secon	<b>Reading</b> Trim 14.2 →	Line Integrals
	Assignment web page $\longrightarrow$	assignment #10

One place that line integrals often come up is in the computation of averages of a function.

2D Case



#### **3D Case**

The temperature in a room is given by T = f(x, y, z). A curve C in the room is given by x(t), y(t) and z(t). If we measure temperature along curve C, what is the average temperature  $\overline{T}$ ?

$$\overline{T} = rac{1}{L} \underbrace{\int_C f(x,y,z)}^{value \ of \ f \ along \ C} \underbrace{\int_C f(x,y,z)}_{line \ integral \ along \ C} \underbrace{dS}_{c}$$



Calculation of the line integral along  $\boldsymbol{C}$ 

$$\int_{t=0}^{\alpha} \underbrace{f[x(t), y(t), z(t)]}_{f \ values \ along \ C} \underbrace{\sqrt{\left(\frac{dx}{dt}\right)^2 + \left(\frac{dy}{dt}\right)^2 + \left(\frac{dz}{dt}\right)^2}}_{dS \ along \ C} \ dt$$

# Example 4.2

Given a 3D temperature field

$$T = f(x, y, z) = 8x + 6xy + 30z$$

find the average temperature,  $\overline{T}$  along a line from (0, 0, 0) to (1, 1, 1).

1. if we have an explicit equation for a planar curve

$$C: \qquad y = g(x)$$

we can reduce

$$\int_C f dS$$
 to  $\int \operatorname{fnc} \operatorname{of} x \ dx$  or  $\int \operatorname{fnc} \operatorname{of} y \ dy$ 

we do not have to always use the parametric equations.

2. value of  $\int_C f \, dS$  depends on (i) function f

(ii) curve C in space

(iii) direction of travel

$$\int_{A}^{B} f \, dS = -\int_{B}^{A} f \, dS$$

3. notation - sometimes C is a closed loop in space



- evaluate once around the loop CCW or CW
- evaluation method is the same as the example

Example: 4.3a

Suppose the temperature near the floor of a room (say at z = 1) is described by

$$T = f(x, y) = 20 - \frac{x^2 + y^2}{3}$$
 where  $-5 \le x \le 5$ 

 $-4 \leq y \leq 4$ 

What is the average temperature along the straight line path from A(0,0) to B(4,3).

## Example: 4.3b

What is the average room temperature along the walls of the room?

$$\overline{T} = rac{\oint_C f(x,y) dS}{\oint_C dS}$$

where the closed curve C is defined in 4 sections

$$egin{array}{rcl} C_1 & y = -4 & x = t & -5 \leq t \leq 5 \ C_2 & x = 5 & y = t & -4 \leq t \leq 4 \ C_3 & y = 4 & x = 5 - t & 0 \leq t \leq 10 \ C_4 & x = -5 & y = 8 - t & 0 < t < 8 \end{array}$$

# Example: 4.3c

What is the average temperature around a closed circular path  $\rightarrow \quad x^2 + y^2 = 9?$ 

where C is a closed circular path

$$\overline{T} = rac{\oint_C f(x,y) dS}{\oint_C dS}$$
 where  $x(t) = 3\cos t$   
 $y(t) = 3\sin t$ 

for  $0 \leq t \leq 2\pi$ .

#### Line Integrals of Vector Functions



Let's examine work or energy in a force field.

$$W=ec{F}\cdotec{d}$$

Now consider a particle moving along a curve C is a 3D force field.

$$W = \int_{C} \underbrace{\vec{F}(x, y, z)}_{force\ value\ evaluated\ along\ C}} \cdot \underbrace{d\vec{r}}_{displacement\ along\ C}} (1)$$

This is a line integral of the vector  $\vec{F}$  along the curve C in 3D space.

In component form:

$$egin{array}{rcl} ec{F}&=&\hat{i}P+\hat{j}Q+\hat{k}R\ dec{r}&=&\hat{i}dx+\hat{j}dy+\hat{k}dz\ W&=\int_{C}Pdx+Qdy+Rdz \end{array}$$

Equations (1) and (2) are equivalent.

Use the equation of curve C (either in an explicit form, i.e. y = f(x) etc., or in a parametric form) to reduce (2) to  $\int_{t=0}^{\alpha} g(t) dt$  or  $\int_{x=n}^{\beta} h(x) dx$  etc.

#### Example 4.4

Given a force field in 3D:

$$ec{F} = \hat{i}(3x^2 - 6yx) + \hat{j}(2y + 3xz) + \hat{k}(1 - 4xyz^2)$$

What is the work done by  $\vec{F}$  on a particle (i.e. energy added to the particle) if it moves in a straight line from (0, 0, 0) to (1, 1, 1) through the force field.

#### Notes

- 1. If we have an explicit equation for the curve, we can sometimes reduce to a form  $\int (\text{fnc of } x) dx$  etc. There is no need for parametric equations.
- 2. The work term W can be either +'ve or -'ve. In a +'ve form, ∫ F and ∫ dr, are in the same direction, where the work done by the force energy is added to the object by F. In the -'ve form, F opposes the displacement. The energy is removed from the object. +'ve W = ∫<sub>C</sub> F · dr
- 3. closed path notation

$$W = \oint_{CCW} \vec{F} \cdot d\vec{r}$$
 once CCW around loop  
 $W = \oint_{CW} \vec{F} \cdot d\vec{r}$  once CW around loop

4. A special case is the conservative force field

$$\oint ec{F} \cdot dec{r} = 0$$

We know that  $\nabla \times \vec{F} = 0$ . There is no work in a closed loop. We also know that  $\nabla \phi = F$ , which is integrated gives

$$\int_C ec{F} \cdot dec{r} = \phi_1 - \phi_2$$

Therefore for a conservative force field, the work is a function of the end points not the path. This is the same for any C connecting the same 2 end points.

W is always the same number if  $\vec{F}$  is conservative.

#### Example: 4.5a

The gravitational force on a mass, m, due to mass, M, at the origin is

$$\vec{F} = -G \frac{Mm\vec{r}}{\left|\vec{r}\right|^3} = -K \frac{\vec{r}}{\left|\vec{r}\right|^3}$$
 where  $K = GMm$ 

The vector field is given by:

$$egin{aligned} ec{F}(x,y,z) &= \hat{i}P + \hat{j}Q + \hat{k}R & ext{where} \quad P &= -rac{Kx}{(x^2+y^2+z^2)^{3/2}} \ Q &= -rac{Ky}{(x^2+y^2+z^2)^{3/2}} \ R &= -rac{Kz}{(x^2+y^2+z^2)^{3/2}} \end{aligned}$$

Compute the work, W, if the mass, m moves from A to B along a semi-circular path in the (y, z) plane:



#### Example: 4.5b

Find the work to move through the same field, but following a straight line path from A(0, 0.1, 1.261) to B(0, 16, 0).



## **Conservative Force Fields**

A space	CALCULUS	<b>Reading</b> Trim 14.5 $\longrightarrow$	Energy and Conservative Force Fields
	Inter-sector Al A Robert And Inter-sector Al A Robert And Inter-	$\begin{array}{l} \textbf{Assignment} \\ \text{web page} \longrightarrow \end{array}$	assignment #10

Given a flow field in 3D space

$$\vec{F} = \hat{i}\underbrace{(2xz^3+6y)}_P + \hat{j}\underbrace{(6x-2yz)}_Q + \hat{k}\underbrace{(3x^2z^2-y^2)}_R$$

**Part a:** Is the force field,  $\vec{F}$ , conservative?

Check to see if  $\nabla \times \vec{F} = 0$  (i.e. irrotational  $\vec{F}$ ?)

**Part b:** Compute the work done on an object if it goes around a CCW circular path of radius 1 for center point P(2, 0, 3) with form

**Part c:** Find the scalar potential function  $\phi(x, y, z)$ 

$$ec{F} = 
abla \phi$$

**Part d:** Use  $\phi$  to verify part b).

$$W=\ointec{F}\cdot dec{r}=\oint 
abla \phi \cdot dec{r}$$

#### Part e:

Find the work done if the object moves along C from A(0,0,0) to B(3,4,-2) within  $ec{F}$ .

## Surface Integrals of Scalar Functions



What is the average temperature measured over the surface z = g(x, y)?

Add up T for each dS area element and divide by the total area of S to get the average.

$$\overline{T} = rac{{\int {\int_S {f(x,y,z)dS} } }}{{Area \ of \ S}}$$

The numerator is called the surface integral of f(x,y,z) over the surface S (i.e. z=g(x,y)). To evaluate

$$\int \int_{S} f dS = \int \int_{\mathcal{R}_{xy}} \underbrace{f[x,y,g(x,y)]}_{T \; values \; on \; the \; surface} \underbrace{\sqrt{1 + \left(rac{\partial g}{\partial x}
ight)^2 + \left(rac{\partial g}{\partial y}
ight)^2} dx dy}_{dS \; area \; element}$$

This becomes

$$\int\!\int_{\mathcal{R}_{xy}}\!F(x,y)dxdy$$

#### Notes

1. sometimes it is easier if we switch to polar coordinates

$$\int \int_{\mathcal{R}_{xy}} F(x,y) dx dy \quad o \quad \int \int_{\mathcal{R}_{xy}} H(r, heta) r dr d heta$$

where  $x = r \cos \theta$  and  $y = r \sin \theta$ .

2. notation = we have a closed surface in space, i.e. a sphere surface

$$g(x,y) 
ightarrow z = \sqrt{a^2 - x^2 - y^2}$$
 $\oint \oint_S f(x,y,z) dS$ 

## Example: 4.6

Suppose the temperature variation (same for all (x, y)) in the atmosphere near the ground is

$$T(z) = 40 - \frac{z^2}{5}$$

where T is in  $^{\circ}C$  and z is in m. Look at a cylindrical building roof as follows:



What is the air temperature in contact with the roof?

# Surface Integrals of Vector Functions



Given a full 3D velocity field,  $\vec{V}(x, y, z)$  in space (i.e. air flow in a room).

Given some surface z = g(x, y) within the flow  $\rightarrow$  calculate the flow rate  $Q(m^3/s)$  crossing the surface S, we can write G = z - g(x, y), where G is a constant since the surface is a level surface or a contour.



The basic idea is to consider the element dS of the surface at some arbitrary (x, y, z). Then compute the unit normal vector to dS

$$\hat{n} = (\pm) rac{
abla G}{|
abla G|}$$

This will vary over S. The  $(\pm)$  will be controlled by the direction of the flow.

The flow across dS is  $(\vec{V} \cdot \hat{n})$  dS.

Add up over all dS elements to get the total flow across the surface

$$Q = \int\!\int_S ec{V} \cdot \hat{n} \ dS$$

This is called the surface integral of the vector field  $\vec{V}$  over the surface S defined by z = g(x, y).

The actual evaluation is similar to the last example.

- $ec{V} \cdot \hat{n}$  will end up giving some integrand function f
- project dS onto (x, y) plane

$$dS = \sqrt{1 + \left(rac{\partial g}{\partial x}
ight)^2 + \left(rac{\partial g}{\partial y}
ight)^2} dx dy$$

$$Q=\int\!\int_{\mathcal{R}_{x,y}}\!f(x,y)\sqrt{1+\left(rac{\partial g}{\partial x}
ight)^2+\left(rac{\partial g}{\partial y}
ight)^2}dxdy$$

• then proceed as before.

## Example: 4.7

Given a velocity field in 3D space

$$ec{V} = \hat{i}(2x+z) + \hat{j}(x^2y) + \hat{k}(xz)$$
 find

- a) the flow rate  $Q(m^3/s)$  across the surface z = 1 for  $0 \le x \le 1$  and  $0 \le y \le 1$  in the +'ve z direction
- b) the average velocity across the surface



## **Integral Theorems Involving Vector Functions**

We will examine vector functions in 3D:

Force Field:  $ec{F}(x,y,z) = \hat{i}P + \hat{j}Q + \hat{k}R$ 

Vector Field:  $ec{V}(x,y,z) = \hat{i}u + \hat{j}v + \hat{k}w$ 

We have defined 2 types of integrals for such functions.

#### **Line Integrals**



$$\int_C ec{F} \cdot dec{r} = \int_C P dx + Q dy + R dz$$

This can be interpreted as work done by  $\vec{F}$  field on an object that moves along C within the field.

**Surface Integrals** 



$$\int \int_S ec{V} \cdot \hat{n} \ dS$$

This can be interpreted as the flow across surface S in the  $\hat{n}$  direction due to the  $\vec{V}$  field.

There are three theorems which state identities involving these types of integrals.

#### 1. Divergence Theorem



where

 $\vec{V}$  = velocity field

 $\mathcal{V}~=~\mathrm{volume}$ 

#### 2. Stokes Theorem

Also called 1st vector from of Green's theorem.

$$\oint_C ec{F} \cdot dec{r} = \int \int_S ( 
abla imes ec{F} ) \cdot \hat{n} \ dS$$

where the surface S is any surface in 3D with C as a boundary.

3. Greens Theorem

This is essentially a 2D statement of Stoke's theorem, where in 2D

$$egin{array}{rcl} ec{F}&=&\hat{i}P+\hat{j}Q \ 
onumber\ &ar{F}&=&\hat{k}\left(rac{\partial Q}{\partial x}-rac{\partial P}{\partial y}
ight) \end{array}$$



 $\vec{F}$  defined in 2D space



Also called Green's theorem in space - this is the 2nd vector form of Green's theorem.

$$\oint \oint_S ec{V} \cdot ec{n} \ dS = \int \int \int_{\mathcal{V}} (
abla \cdot ec{V}) d\mathcal{V}$$

## **Divergence** Theorem



Trim in section 14.9 has a detailed proof of the Divergence Theorem. They try to interpret the meaning of

$$\oint \oint_S ec{V} \cdot \hat{n} dS = \int \int \int_{\mathcal{V}} (
abla \cdot ec{V}) d\mathcal{V}$$

This equation applies for any vector function  $\vec{V}$ , but is used most for velocity fields in fluids. When we consider  $\vec{V}$ , the theorem concerns net outflow to inflow  $(m^3/s)$  for a region in space (like a sphere).

The left side of the equation is a surface integral of V over a closed surface, S in 3-D space with  $\hat{n}$  being the outward normal to each dS.

We recall that  $\vec{V} \cdot \hat{n} dS$  gives the flow rate  $(m^3/s)$ . When we add this up over the entire surface (as in the LHS of the equation) we obtain the **net flow rate crossing the closed surface**.

i.e.

net outward flow
$$(m^3/s)$$
 – net inward flow $(m^3/s)$ 

The right hand side of the equation is a calculation of  $\nabla \cdot \vec{V}$  for each differential volume,  $d\mathcal{V}$  inside the surface S. We then add them all up.

For the differential volume,  ${m {\cal V}}$ 

$$\begin{array}{lll} \mathrm{inflow}\;(m^3/s)\;\;=\;\;u(x)\cdot area+v(y)(\Delta x)(\Delta z)\\ \mathrm{outflow}\;(m^3/s)\;\;=\;\;u(x+\Delta x)\cdot(\Delta y)(\Delta z)+v(y+\Delta y)(\Delta x)(\Delta z) \end{array}$$

The net flow is then

$$ext{outflow} - ext{inflow} = (\Delta x)(\Delta y)(\Delta z) \left[ rac{u(x+\Delta x)-u(x)}{\Delta x} + rac{v(y+\Delta y)-v(y)}{\Delta y} 
ight]$$

$$egin{array}{lll} &=& (d\mathcal{V})\left(rac{\partial u}{\partial x}+rac{\partial v}{\partial y}
ight) \ &=& (
abla\cdotec V\cdotec V)d\mathcal{V} \end{array}$$

Therefore the RHS  $(\nabla \cdot \vec{V}) d\mathcal{V}$  gives the net outflow minus inflow for a volume element  $d\mathcal{V}$ .

The integral  $\int \int \int_{\mathcal{V}}$ , adds up the differential flow for all volume elements,  $d\mathcal{V}$  inside of surface S. There is a cancellation of terms because the outflow from one  $\Delta \mathcal{V}$  becomes the inflow to the next volume.

When we sum over all  $\Delta \mathcal{V}$ , we are left with the difference between the inflow and the outflow at the boundaries of the volume.

$$\oint \oint_S \vec{V} \cdot \vec{n} dS = \int \int \int_{\mathcal{V}} (\nabla \cdot \vec{V}) d\mathcal{V}$$
  
outflow - inflow $(m^3/s)$  triple sum of all outflow - inflow  
across boundary surface for  $\Delta \mathcal{V}$  volumes inside  
 $S$  of volume  $\mathcal{V}$  in 3D space the volume  $\mathcal{V}$  in 3D space

#### Example: 4.8

Given

$$ec{V} = \hat{i}(1+x) + \hat{j}(1+y^2) + \hat{k}(1+z^3)$$

verify the divergence theorem for a cube, where  $0 \leq x, y, z \leq 1$  i.e. show that

$$\oint \oint_S ec{V} \cdot \hat{n} dS = \int \int \int_{\mathcal{V}} (
abla \cdot ec{V}) d\mathcal{V}$$

where

S = cube surface (closed)

 $\mathcal{V}$  = interior volume of the cube

## Stoke's Theorem



The formal proof is offered in Trim 14.10.

$$\oint_C ec{F} \cdot dec{r} = \int \int_S (
abla imes ec{F}) \cdot \hat{n} \ dS$$

This has a similar meaning to Green's theorem but now in 3D space instead of a plane.



 $\vec{F}(x, y, z)$  is a 3D force field. The LHS of the equations is the work done when the object moves once in a CCW direction along the path *C* in 3D. The RHS is the work computed over a surface integral  $\int \int_{S}$ .

Like Greens theorem, it works because of the interior cancellations of work, when we move around a surface element dS inside C.

Note: the unit normal,  $\hat{n}$  for the LHS is based on a right hand rule as follows.



The work on all internal surfaces cancel, leaving only the surface work in the CCW direction.

# Example: 4.9

Given:  $\vec{F} = \hat{i}x + \hat{j}2z + \hat{k}y$  (a force field in 3D).

The closed path  $\boldsymbol{C}$  is given by the intersection of:

$$\begin{array}{rcl} x^2+y^2&=&4\\ &z&=&4-x-y \end{array}$$

The object moves once in a CW direction around C starting at (2, 0, 2).

Verify Stoke' theorem:

$$\oint_C ec{F} \cdot dec{r} = \int \int_S (oldsymbol{
abla} imes ec{F}) \cdot \hat{n} \ dS$$

## Green's Theorem



The theorem involves work done on an object by a 2D force field. The 2D force field is given by

$$F(x,y)=\hat{i}P(x,y)+\hat{j}Q(x,y)$$



of C. The theorem states

$$\oint_C P dx + Q dy = \int \int_{\mathcal{R}} \left( rac{\partial Q}{\partial x} - rac{\partial P}{\partial y} 
ight) dx dy$$

The left hand side of the equation,  $\oint_C \vec{F} \cdot d\vec{r}$  in 2D is the work done by the field  $\vec{F}$  on the object as it moves on C. This consists of force times distance for each  $d\vec{r}$  added up over C.



Q

Ρ

R

С

The **right hand side** of the equation,  $\int \int_{\mathcal{R}} (\nabla \times \vec{F}) \cdot$  $\hat{k}dxdy$  in 2D gives the direction of travel on C for the work given by the LHS. Maps movement of an element  $\Delta x \Delta y$  as it moves around from A to A.





$$Work = Q|_{at x + \Delta x} \Delta y - P|_{at y + \Delta y} \Delta x - Q|_{at x} \Delta y + P|_{at y} \Delta x$$
$$= (\Delta x \Delta y) \left[ \frac{Q|_{at x + \Delta x} - Q|_{at x}}{\Delta x} - \frac{P|_{at y + \Delta y} - P|_{at y}}{\Delta y} \right]$$

In the limit, the work done by  $\vec{F}$  to move the object CCW around dxdy area is

$$\left(rac{\partial Q}{\partial x}-rac{\partial P}{\partial y}
ight)dxdy$$

gives the work done.

Now we can sum up for all dxdy elements inside C.



There are some cancellations (+) (-) for all interior  $\Delta x, \Delta y$  paths. Therefore when we do  $\oint \oint_{\mathcal{R}}$ , we are left with the work terms on the boundaries of  $\mathcal{R}$ .

$$\oint_C P dx + Q dy \;\; = \;\; \int \int_{\mathcal{R}} \left( rac{\partial Q}{\partial x} - rac{\partial P}{\partial y} 
ight) dx dy$$

work when we

sum of all work if

move once CCW around move once CCW around all

> boundary curve C(dxdy) area elements of  ${\cal R}$

> > inside C

# Example: 4.10

Given a 2D force field,  $ec{F}(x,y) = \hat{i}(xy^3) + \hat{j}(x^2y)$  and a path C in the field:

Verify Green's theorem

$$\oint_C P dx + Q dy = \int \int_{\mathcal{R}} \left( rac{\partial Q}{\partial x} - rac{\partial P}{\partial y} 
ight) dx dy$$

with

$$P = xy^3$$
  
 $Q = x^2y$